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Contact and Interface Mechanics: Modeling and Computation Hyper-dimensional Gap Finite Elements for the Enforcement of Interfacial Constraints



#### Outline

- 1. Limitations of conventional contact algorithms
- 2. The proposed contact discretization methodology
- 3. Distinguishing novelties and potential advantages
- 4. Demonstration of efficacy and preliminary results
- 5. Conclusions and future work

### Conventional contact enforcement methods possess several critical limitations



#### Node-to-surface methods:

- Non-symmetric behavior
- Non-smooth sliding (chatter)
- Poor solution accuracy (locking)



#### Surface-to-surface methods:

- Computationally expensive
- Difficult to implement
- Not easily generalized

Mathematical statement of contact problems necessitates the definition of well-defined shared interfaces/boundaries between continuum bodies

#### Model problem

"Tied" interface constraint:

$$x_1 - x_0 = \mathbf{0} \quad \forall x \in \Gamma$$

Enforcement using Lagrange multipliers:

$$\int_{\Gamma} (\boldsymbol{x}_1 - \boldsymbol{x}_0) \cdot \boldsymbol{\lambda} \, \mathrm{d}\Gamma = 0 \quad \forall \boldsymbol{\lambda}$$



### Shared interface is ambiguously defined in a finite element discretization of the original BVP

- A discrete intermediate surface is defined
  - Chosen somewhat **arbitrarily**
- Point pairs on both bodies are related through a projective mapping
  - Computationally expensive
  - Mapping is not always unique or robust

$$\int_{\Gamma^h} (x_1 - x_0) \cdot \lambda \,\mathrm{d}\Gamma^h = 0 \quad \forall \lambda$$



### Define a continuous family of intermediate surfaces parameterized by $\alpha \in [0,1]$

- Regard  $\alpha$  as an auxiliary spatial coordinate

 $\chi = (x, \alpha)$ 

• Mortar constraint integrals may be evaluated over a specific intermediate surface  $\Gamma_{\alpha}$ 

$$\int_{\Gamma_{\alpha}} (\boldsymbol{x}_1 - \boldsymbol{x}_0) \cdot \boldsymbol{\lambda} \, \mathrm{d}\Gamma_{\alpha} = 0 \quad \forall \boldsymbol{\lambda}$$



### Define a local measure of separation between adjacent intermediate surfaces parameterized by $\alpha$

$$(x_1 - x_0) = 0 \quad \forall x \in \Gamma$$
$$\frac{\partial x}{\partial \alpha} = 0 \quad \forall x \in \Gamma_{\alpha}$$

$$\frac{\partial x}{\partial \alpha} = \lim_{\Delta \alpha \to 0} \frac{x_{\alpha + \Delta \alpha} - x_{\alpha}}{\Delta \alpha}$$



Pose mortar integrals over the intermediate domain  $\Sigma$  comprising all intermediate surfaces  $\Gamma_{\alpha}$ 

$$\int_{\Gamma} (x_1 - x_0) \cdot \lambda \, \mathrm{d}\Gamma = 0 \quad \forall \lambda$$

$$\int_{\alpha=0}^{\alpha=1} \int_{\Gamma_{\alpha}} \frac{\partial x}{\partial \alpha} \cdot \lambda \, \mathrm{d}\Gamma_{\alpha} \, \mathrm{d}\alpha = 0 \quad \forall \lambda$$

• Regard  $\Sigma$  as a differentiable manifold  $\Sigma = \{\Gamma_{\alpha} \mid \forall \alpha \in [0,1]\}$ 

 $\mathbf{X}_1$ n α  $\mathbf{X}_{0}$  $\Gamma_0$  $\Omega_0$ 

### Represent $\Sigma$ parametrically as an *n*-dimensional hyper-surface embedded in $\mathbb{R}^{n+1}$



Projection of the directed hyper-surface area  $d\Sigma$ onto the original spatial domain yields the desired differential form for evaluating mortar integrals



#### The intermediate surface normal n may further be used to enforce normal contact constraints



#### Exploit a conformal discretization of the intermediate domain into finite elements

FEM basis:  $\boldsymbol{\chi} = \sum_{\forall a} \varphi_a \, \boldsymbol{\chi}_a$ a



# Select the Lagrange multiplier basis consistent with $L^2$ minimization of $\frac{\partial x}{\partial \alpha}$ over the intermediate domain





### The proposed approach differs from other related volume-based interface discretization methods

- 1. The contact domain method (Oliver et al., 2009)
- 2. The third medium approach (Wriggers et al., 2013)
- 3. Contact layer elements (Weißenfels and Wriggers, 2015)
- 4. Fictitious contact material method (Bog et al., 2015)

Introduction of the hyper-dimensional coordinate  $\alpha$  constitutes a distinguishing novelty of the method

#### Tied patch tests: errors on the order of machine precision for linear/quadratic elements in 2D/3D



#### Pressurized cylinder: $L^2$ and $H^1$ errors converge at expected rates using linear/quadratic elements



### Stacked cantilever beam: finite deformations with moderate sliding, showing locking-free behavior



#### The proposed method offers several advantages

- 1. Does not require the computation of geometric intersections or projections
  - -Requires conformal meshing of the intermediate domain
- 2. Standard Gaussian quadrature is sufficient for satisfaction of patch tests and convergence
- 3. Natural and efficient extension to higher-order discretizations

## Ongoing and future work will seek to explore the following areas of continuing interest:

- Large sliding problems with separation and friction
- Stable symmetric dual-pass mortar formulations
- Surface-to-surface mesh solution remapping
- Locking-free penalty formulations
- Alternative discretization methods:
  - Isogeometric surfaces
  - Boundary element method
  - Polyhedral elements
  - Mesh-free methods
  - ALE methods

### Questions?